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# What is Diffusion?

In earlier publications, heat Q<sup>-</sup> is defined as an interaction that is entirely distinguishable from work W<sup>-</sup>. The energy exchanged Q<sup>-</sup> is T<sub>Q</sub> times the entropy exchanged S<sup>-</sup>, where T<sub>Q</sub> is the almost common temperature of the interacting systems. Here, we define diffusion as another interaction that is entirely distinguishable from both work and heat, and that involves exchanges of energy, entropy, and amount of a constituent. It is an interaction between two systems A and B that pass through stable equilibrium states while their respective parameters remain fixed, and that have almost equal temperatures T<sup>A</sup>  $\approx$  T<sup>B</sup>  $\approx$  T<sub>D</sub> and almost equal total potentials  $\mu^{A} \approx \mu^{B} \approx \mu_{D}$  of the diffusing constituent. The exchanges of entropy S<sup>-</sup>, energy E<sup>-</sup>, and amount of constituent n<sup>-</sup> out of one system satisfy the relation S<sup>-</sup> = (E<sup>-</sup>  $- \mu_{D}$ n<sup>-</sup>)/T<sub>D</sub>. In the limit of n<sup>-</sup> = 0, a diffusion interaction becomes heat.

System A

State A<sub>4</sub>

E,<sup>A</sup> , n,<sup>A</sup>

T1<sup>A</sup> , μ1<sup>A</sup>

## **1** Introduction

In some expositions of thermodynamics, the concept of diffusion is assumed self-evident and not defined explicitly (Katchalsky and Curran, 1967; and Chartier et al., 1975). In other expositions, diffusion in the widest sense is "the macroscopically perceptible relative motion of individual particles" (Chapman and Cowling, 1964; and Haase, 1969a), or "the transport of matter caused by concentration gradients" (Haase, 1969b). From these definitions, it is not clear whether diffusion should be viewed as an interaction at a boundary of a system or as a property of a system.

Consistent with our earlier discussions of work, heat, and bulk-flow interactions (Gyftopoulos and Beretta, 1991a), in this paper we define diffusion as an interaction occurring at a boundary of a system that is entirely distinguishable from work, and that involves exchanges of energy, entropy, and amounts of constituents between which exists a specified relation.

The paper is organized as follows: nonwork interactions are discussed in Section 2, diffusion is defined in Section 3, and conclusions are presented in Section 4.

#### 2 A Nonwork Interaction

An interaction that cannot be classified as work is called nonwork (Gyftopoulos and Beretta, 1991b). An example of a nonwork interaction is heat (Gyftopoulos and Beretta, 1991c; and Beretta and Gyftopoulos, 1990). Another is the interaction between two systems A and B that experience a process under the following specifications (Fig. 1). Each system consists of at least one common constituent and, initially, is in a stable equilibrium state, but not in mutual stable equilibrium with the other because the initial temperature  $T_1^A$  at state  $A_1$  differs from the initial temperature  $T_1^B$  at state  $B_1$ , and for the common constituent the initial total potential  $\mu_1^A$  differs from the initial total potential  $\mu_1^B$ . At the end of the process, the states  $A_2$  and

Initial States System A System B State  $A_2$   $E_1^A + DE^A$   $n_1^A + Dn^A$ Final States Fig. 1  $B_2$  are not necessarily stable equilibrium, the energy as

 $B_2$  are not necessarily stable equilibrium, the energy and amount of constituent of system A are changed, the changes in energy and amount of constituent of system B are, respectively, equal and opposite to those of A, no net effects are left on the parameters and other constituents of either A or B, and no net effects are left on any system in the environment of the composite of systems A and B. Under these specifications, the interaction between A and B is nonwork because it involves exchanges of both energy and amount of the common constituent. In general, however, this interaction can be regarded as partly nonwork and partly work. To see this clearly, we reproduce the process just cited in two steps.

In the first step, we interpose between A and B a cyclic engine  $X_1$  that produces shaft work without any entropy generation by irreversibility (Fig. 2(a)). The cyclic engine can do

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System B

State B

E<sub>1</sub><sup>B</sup>, n<sub>1</sub><sup>B</sup>

Τ,<sup>Β</sup>, μ,<sup>Β</sup>

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#### Nomenclature -

- A = system
- $A_i$  = state *i* of system A
- B = system
- $B_i$  = state *i* of system B $dE^A$  = infinitesimal change of energy of A
- $DE^X$  = change of energy of system X
- $dn^A$  = infinitesimal change of amount of constituent of A
- $Dn^X$  = change of amount of constituent of system X $DS^X$  = change of entropy of
- $E^{-} =$ flow of energy, positive if out of a system
- $E_i^X$  = energy of system X in state *i*
- $E^{X-}$  = flow of energy, positive if into system X  $E^{X-}$  = flow of energy. posi-
- $E^{X-}$  = flow of energy, positive if out of system X g = gravity acceleration

 $S^X(E^X, n^X)$ 

 $T_D =$ 

- h = specific enthalpy
- $n^-$  = flow of amount of

work because the composite of systems A and B is not in a stable equilibrium state  $(T_1^A \neq T_1^B \text{ and } \mu_1^A \neq \mu_1^B)$ , and, therefore, its adiabatic availability is different from zero. The changes involved in the first step are as follows:

(a) Transfers of energy, amount of the common constituent, and perhaps entropy out of system A and into the cyclic engine  $X_1$  equal to the respective transfers experienced in the course of the original nonwork interaction. As a result of these transfers and possibly internal effects, system A changes from state  $A_1$  to its final state  $A_2$ , the state reached in the original nonwork process.

(b) Transfer of some of the energy received by  $X_1$  to a weight—shaft work done to raise the weight.

(c) Transfer of the remaining energy received by  $X_1$ , and transfers of all the amount of constituent and entropy received by  $X_1$  to system *B*. As a result of these transfers only, system *B* reaches an intermediate state  $B_3$  different from the final state  $B_2$  reached in the course of the original process because less energy is exchanged between  $X_1$  and *B* than between *A* and *B*. Moreover, here the interaction between  $X_1$  and *B* must be viewed as nonwork because it involves both energy and an amount of the constituent.

In the second step, we disconnect systems A and  $X_1$ , and connect the raised weight to a cyclic engine  $X_2$  that can do work on system B while the weight is lowered to its initial elevation (Fig. 2(b)), and do so without generating any entropy by irreversibility. As a result of the shaft work done on B and possibly internal effects, system B is carried from state  $B_3$  to the final state  $B_2$  reached by system B in the course of the original nonwork process.

At the completion of the two steps, 1) both cyclic engines  $X_1$  and  $X_2$ , and the weight are restored to their respective initial states; 2) systems A and B experience the same changes of states—exchange the same amounts of energy, constituent, and perhaps entropy as in the original process, and generate the same amounts of entropy; and 3) we conclude that the in-

constituent, positive if		of temperatures of sys-
flow of amount of		fusion interaction
constituent positive if	$T_{\alpha}$ -	almost common tem
out of a system	ΥŲ –	peratures of systems
flow of constituent		experiencing heat inter-
positive if into system		action
X	$T^X =$	temperature of system
flow of constituent	1 -	Y
positive if out of	$T_{i}^{X} =$	temperature of system
system X	1, -	X in state <i>i</i>
amount of constituent	$W^{\neg} =$	work positive if done
of system $X$ in state $i$	<i>,, _</i>	hy a system
heat, positive if into a	<i>X</i> . =	cyclic engine <i>i</i>
system	$M_1 =$	almost common value
specific entropy	μD	of total potentials of
flow of entropy posi-		systems experiencing
tive if into a system		diffusion interaction
flow of entropy posi-	11 in -	almost common value
tive if out of a system	$\mu_{iD} =$	of total potentials of
flow of entropy posi-		ith constituent of sys
tive if into system X		tems experiencing dif
flow of entropy posi-		fusion interaction
tive if out of system Y	$u^{x}$ –	total potential of sys
entropy of system X in	μι —	tem V in state i
state i	"× _	total potential of
fundamental relation	μ –	system V
of system X	٤	speed of hulk flow
almost common value	ς	speed of our now
unitoff common value		State

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teraction between the two systems initially at different temperatures and different total potentials can be regarded partly as nonwork (step 1), and partly as work (step 2). The question now arises "Is this conclusion always valid?" We examine the answer to this question in the next section.

## **3** Diffusion

Here we discuss a special nonwork interaction that involves at least exchanges of both energy and amount of a constituent, and yet is entirely distinguishable from work in that no fraction of any such interaction can be regarded as work. To proceed, we first evaluate the work done by the cyclic engine  $X_1$  and the systems in Fig. 2(a) in a reversible weight process for the composite of systems A, B, and cyclic engine  $X_1$ . In this process, the initial states  $A_1$  and  $B_1$  are stable equilibrium, the final states  $A_2$  and  $B_3$  are not necessarily stable equilibrium, and there are no net changes in parameters and other constituents of either system A or system B.

Under these conditions, and for given changes  $DE^A$ ,  $DS^A$ , and  $Dn^A$ , respectively, in the energy, entropy, and amount of constituent of system A, or flows  $E^{A^-}$ ,  $S^{A^-}$ , and  $n^{A^-}$  out of system A, the corresponding energies  $E_2^A$  and  $E_3^B$ , entropies  $S_2^A$ and  $S_3^B$ , and amounts of constituents  $n_2^A$  and  $n_3^B$  of states  $A_2$ and  $B_3$ , respectively, and the energies  $E_1^A$  and  $E_1^B$ , entropies  $S_1^A$ and  $S_1^B$ , and amounts of constituents  $n_1^A$  and  $n_1^B$  of the initial states  $A_1$  and  $B_1$ , respectively, satisfy the relations

$$E_2^A = E_1^A + DE^A = E_1^A - E^{A \to} \quad E_3^B = E_1^B + DE^B = E_1^B + E^{B \to}$$
(1)

$$S_2^{\mathcal{A}} = S_1^{\mathcal{A}} + DS^{\mathcal{A}} = S_1^{\mathcal{A}} - S^{\mathcal{A}} - S_3^{\mathcal{B}} = S_1^{\mathcal{B}} + DS^{\mathcal{B}} = S_1^{\mathcal{B}} + S^{\mathcal{B}} - (2)$$

$$n_2^A = n_1^A + Dn^A = n_1^A - n^{A-} \quad n_3^B = n_1^B + Dn^B = n_1^B + n^{B-} \quad (3)$$

where, in writing the second of Eqs. (3), we use the fact that no amount of constituent flows to the weight,  $DE^B$  and  $DS^B$ are, respectively, the changes in energy and entropy between states  $B_3$  and  $B_1$ , and a superscript with an arrow pointing to the right indicates positive flow out of the system. If the arrow points to the left, then positive flow is into the system.

By virtue of the highest-entropy principle (Gyftopoulos and Beretta, 1991d), the entropy  $S_2^A$  cannot be larger than the entropy of the stable equilibrium state corresponding to the same values of energy and amount of the common constituent as those of state  $A_2$ . Similarly,  $S_3^B$  cannot be larger than the entropy of the stable equilibrium state corresponding to the same values of energy and amount of the common constituent as those of state  $B_3$ . Moreover, by virtue of the state principle (Gyftopoulos and Beretta, 1991e), the two highest entropies are functions of the forms  $S^A(E^A, n^A)$  and  $S^B(E^B, n^B)$ , respectively, where we omit the dependences on parameters and other constituents because here the values of the parameters and the amounts of the other constituents experience no changes. So, we have the relations

$$S_2^A \le S^A(E_2^A, n_2^A) \text{ and } S_3^B \le S^B(E_3^B, n_3^B)$$
 (4)

where the equal sign of the first or second relation holds only if the final state  $A_2$  or  $B_3$  is stable equilibrium, respectively.

To find the work, in addition to relations (1) to (4), we consider the energy and entropy balances for the reversible process of the composite of systems A, B, and  $X_1$ ; that is,

$$DE^{A} + DE^{B} = E_{2}^{A} - E_{1}^{A} + E_{3}^{B} - E_{1}^{B} = -W^{-}$$
(5)

$$DS^{A} + DS^{B} = S_{2}^{A} - S_{1}^{A} + S_{3}^{B} - S_{1}^{B} = 0$$
 (6)

where  $W^{\rightarrow}$  is the work done on the weight.

The value of the work depends on the types of the final states  $A_2$  and  $B_3$ . Indeed, upon combining relations (4) and Eq. (6), we find

$$S_{1}^{A} + S_{1}^{B} = S_{2}^{A} + S_{3}^{B} \le S_{2}^{A} + S^{B}(E_{3}^{B}, n_{3}^{B}) \le S^{A}(E_{2}^{A}, n_{2}^{A}) + S^{B}(E_{3}^{B}, n_{3}^{B})$$
(7)

where the first inequality becomes an equality only if state  $B_3$ 

is stable equilibrium, and the second only if state  $A_2$  is stable equilibrium. From relations (7), we conclude further that

$$S_1^{A} + S_1^{B} - S^{A} (E_2^{A}, n_2^{A}) \le S_1^{A} + S_1^{B} - S_2^{A} \le S^{B} (E_3^{B}, n_3^{B})$$
(8)

where the first inequality becomes an equality only if state  $A_2$  is stable equilibrium, and the second only if state  $B_3$  is stable equilibrium. Moreover, using Eqs. (1) and (5) in relations (8), we find

$$S_{1}^{A} + S_{1}^{B} - S^{A} \left( E_{1}^{A} + DE^{A}, n_{1}^{A} + Dn^{A} \right) \le S_{1}^{A} + S_{1}^{B} - S_{2}^{A}$$
$$\le S^{B} \left( E_{1}^{B} - DE^{A} - W^{-}, n_{1}^{B} - Dn^{A} \right) \quad (9)$$

For given initial states  $A_1$  and  $B_1$ , and given changes in energy,  $DE^A$ , and in amount of constituent,  $Dn^A$ , we observe that the left-hand side of relations (9) has a fixed value. This is the smallest value that can be achieved by  $S_1^A + S_1^B - S_2^A$ , and can be assumed by  $S^B(E_1^B - DE^A - W^-, n_1^B - Dn^A)$  only if both states  $A_2$  and  $B_3$  are stable equilibrium. Next, we recall that the fundamental relation  $S^B(E_1^B - DE^A - W^-, n_1^B - Dn^A)$  is monotonically decreasing with  $E^B$ . It follows that  $S^B(E_1^B - DE^A - W^-, n_1^B - Dn^A)$  is the largest only if  $S^B(E_1^B - DE^A - W^-, n_1^B - Dn^A)$  is the smallest; that is, only if both states  $A_2$  and  $B_3$  are stable equilibrium.

For infinitesimal changes in energy,  $dE^A$ , and amount of constituent,  $dn^A$ , we can find an explicit expression for the largest work  $(W^-)_{\text{largest}}$ . Indeed, upon expanding  $S^A$  in the first relation (9) into a Taylor series around  $E_1^A$  and  $n_1^A$ , and upon expanding  $S^B$  in the second relation (9) into a Taylor series around  $E_1^B$  and  $n_1^B$ , and retaining only first-order terms in these expansions, we find

$$S^{A}(E_{1}^{A} + dE^{A}, n_{1}^{A} + dn^{A}) = S_{1}^{A} + \frac{1}{T_{1}^{A}} dE^{A} - \frac{\mu_{1}^{A}}{T_{1}^{A}} dn^{A}$$
(10)

and

$$S^{B}(E_{1}^{B} - dE^{A} - W^{-}, n_{1}^{B} - dn^{A}) = S_{1}^{B} + \frac{1}{T_{1}^{B}} (-dE^{A} - W^{-}) + \frac{\mu_{1}^{B}}{T_{1}^{B}} dn^{A}$$
(11)

where  $1/T = \partial S/\partial E$ , and  $\mu/T = -\partial S/\partial n$ . Upon substituting Eqs. (10) and (11) into relations (9), and rearranging terms, we find

$$\frac{1}{T_1^B} W^{-} \le \left(\frac{1}{T_1^B} - \frac{1}{T_1^A}\right) (-dE^A) + \left(\frac{\mu_1^B}{T_1^B} - \frac{\mu_1^A}{T_1^A}\right) dn^A \quad (12)$$

Clearly, the largest work is done only if the equal sign applies, that is, only if the final states  $A_2$  and  $B_3$  are stable equilibrium, so that

$$\frac{1}{T_1^B} (W^-)_{\text{largest}} = \left(\frac{I}{T_1^B} - \frac{1}{T_1^A}\right) E^{A^-} - \left(\frac{\mu_1^B}{T_1^B} - \frac{\mu_1^A}{T_1^A}\right) n^{A^-}$$
(13)

where in writing the right-hand side of Eq. (13), we use the notation introduced in Eqs. (1) to (3).

Equation (13) indicates that if the initial temperature  $T_1^A$  and the initial ratio  $\mu_1^A/T_1^A$  of system A differ from the initial temperature  $T_1^B$  and the initial ratio  $\mu_1^B/T_1^B$  of system B, respectively, a fraction of the energy  $E^{A-}$  plus an energy-equivalent fraction of the amount of constituent  $n^{A-}$  transferred out of system A can always be transferred to a weight, while the remainders of these fractions are transferred to system B. The energy stored in the weight can always be returned to B by means of a weight process. Thus, system B appears to experience an interaction which is partly nonwork and partly work.

But if the two initial temperatures are almost equal, and the two initial total potentials are almost equal,  $(W^-)_{\text{largest}}$  approaches zero faster than both  $E^{A-}$  and  $n^{A-}$ , and the interaction between A and B is entirely distinguishable from work in that no fraction of such an interaction can be regarded as work, even if we interpose a cyclic engine between the two interacting systems.

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Table 1 Exchanges in four different interactions

	Interaction				
Exchange	Work Heat		Bulk flow <sup>(a)</sup>	Diffusion	
Energy	₩¬	Q-	$\left(h+\frac{\xi^2}{2}+gz\right)n^{-1}$	$E^{-}$	
Entropy	0	$\frac{Q^{-}}{T_{O}}$	sn <sup>-</sup>	$\frac{E^ \mu_D n^-}{T_D}$	
Constituent	0	0	n	n	

<sup>(a)</sup>The specific enthalpy h and specific entropy s refer to the stable equilibrium state part of the bulk flow state (Gyftopoulos and Beretta, 1991a). The speed  $\xi$ , and elevation z in the gravity field g refer to the mechanical features of the bulk flow state. Flow of the constituent is into the system if  $n^-$  is positive.

In this limit, Eqs. (10) and (11) yield

$$S^{A^{-}} = S_{1}^{A} - S^{A} (E^{A} + dE^{A}, n_{1}^{A} + dn^{A})$$
$$= -\frac{dE^{A} - \mu_{D} dn^{A}}{T_{D}} = \frac{E^{A^{-}} - \mu_{D} n^{A^{-}}}{T_{D}} \quad (14)$$

$$S^{B-} = S^{B}(E_{1}^{B} - dE^{A}, n_{1}^{B} - dn^{A}) - S_{1}^{B}$$
$$= -\frac{dE^{A} - \mu_{D}dn^{A}}{T_{D}} = S^{A-} \quad (15)$$

where  $T_D$  is the almost common value of the initial temperatures  $T_1^A$  and  $T_1^B$ , and  $\mu_D$  the almost common value of the initial total potentials  $\mu_1^A$  and  $\mu_2^B$  of the interacting systems A and B.

An interaction resulting in net exchanges of entropy, energy, and amount of a constituent between two systems A and Bthat are in stable equilibrium states at almost equal temperatures, and almost equal total potentials, and such that the flows of entropy  $S^{4-}$ , energy  $E^{4-}$ , and amount of constituent  $n^{A-1}$  out of system A are related by the last of Eqs. (14); that is,

$$S^{A-} = \frac{E^{A-} - \mu_D n^{A-}}{T_D} \tag{16}$$

is what we call *diffusion*. Thus, diffusion is not a property of a system, nor is it contained in a system. It is an interaction that involves transfers of energy, entropy, and amount of a constituent that are related by Eq. (16). Such an interaction is entirely distinguishable from work.

For comparison, the exchanges of energy, entropy, and amount of constituent in work, heat, bulk flow, and diffusion interactions are listed in Table 1.

In the limit of  $n^- = 0$ , a diffusion interaction becomes a heat interaction.

A diffusion interaction can be generalized to more than one constituent. If two systems A and B, each consisting of rconstituents denoted by subscripts 1, 2, ..., r, are in stable equilibrium states at almost the same temperature  $T_D$ , and at almost the same total potentials  $\mu_{1D}$ ,  $\mu_{2D}$ , ...,  $\mu_{rD}$ , and such

that the flows of entropy  $S^{A-}$ , energy  $E^{A-}$ , and amounts of constituents  $n_1^{A-}$ ,  $n_2^{A-}$ , ...,  $n_r^{A-}$  out of system A satisfy the relation

$$S^{A-} = \frac{E^{A-} - \Sigma_{i=1}^{r} \mu_{iD} n_{i}^{A-}}{T_{D}}$$
(17)

then the interaction is called *multiconstituent diffusion* or, simply, diffusion.

It can be readily shown that two or more diffusion interactions are very useful in discussions of heat conduction, flow of neutral particles through a medium, such as neutrons in nuclear reactors, flow of electrons in an electric circuit, and thermoelectricity, that is, in discussions of transport phenomena. For example, by considering a cubical piece of material in a steady state resulting from six diffusion interactions, one at each of the six interfaces, we can combine the amount of constituent (mass), the energy, and the entropy balances and express the entropy generation in the material in terms of fluxes and forces defined by the characteristics of the diffusion interactions.

#### 4 Conclusions

Diffusion is another ingenious thermodynamic concept that allows the quantitative distinction between entropy generated by irreversibility and entropy exchanged via interactions. By itself or combined with work, heat, and bulk-flow interactions in writing the energy, entropy, and mass balances, diffusion provides us with practical means for identifying opportunities to reduce the entropy generated by irreversibility and, hence, to improve the performance of a system. These opportunities could be missed if the definition of diffusion were ambiguous.

The proposed definition is consistent with the requirements of the phenomenological equations discussed under the headings of either irreversible thermodynamics or transport phenomena.

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